Effect of NaNO₃ Addition on the Decomposition of RuCl₃ Supported on Alumina

INTRODUCTION

Ruthenium is one of the most active catalyst for hydrogenation of carbon oxides and for many other reactions (1-4). The Ru catalysts are sometime modified by the addition of alkali promoter, and catalyst performances of these alkali-promoted catalysts have been widely examined (5-11).

During the course of our study on the syngas conversion on alkali-promoted Ru catalysts (12, 13), we found that the performance of alkali-promoted Ru catalyst prepared from NaNO3 and commercial "RuCl3 · 3H₂O'' was strongly affected by its preparation conditions. Although detail investigation on the preparation of supported or unsupported Ru catalyst have appeared (14-18), preparation of alkali-promoted catalyst have not been dealt until quite recently where reduction of unsupported RuCl₃-CsNO₃ mixture was examined in some detail (19). Therefore, we examined the effects of NaNO₃ addition upon the thermal decomposition and reduction of alumina-supported Ru catalyst.

EXPERIMENTAL

Alumina-supported RuCl₃-NaNO₃ samples with varying NaNO₃ concentration (samples 1–10, Table 1) were prepared by impregnation of a predried alumina (2 g, γ -form, 82 m²/g, 20–35 μ m, obtained by 700°C calcination of well-crystallized boehmite (20)) with 2 ml of an aqueous solution of commercial "RuCl₃ · 3H₂O" (Mitsuwa) and NaNO₃ followed by drying in air at room temperature with continuous stirring. The concentration of RuCl₃ was arbitrarily fixed to give 4% Ru in reduced catalysts.

RESULTS AND DISCUSSION

Thermal Decomposition

In a series of experiments, thermal decomposition up to 400°C was examined with the aid of a thermal analyzer (Shimazdu DTA-30), and the following observations were noted (Table 1). (a) When NaNO₃ and RuCl₃ were coimpregnated, two weight loss processes were detected, one at around 240°C, and the other at around 380°C (Fig. 1b). (b) The higher temperature weight loss took place at the similar temperature range as recorded for $RuCl_3/Al_2O_3$ (sample 1, see Fig. 1a). (c) The lower temperature weight loss process was an endothermic one which consumed significantly larger amounts of heat than the higher temperature weight loss process (Fig. 1). (d) The degree of weight loss at the lower temperature as well as the intensity of the associated endothermic peak increased with an increase in NaNO₃ loading until Na/Cl ratio became unity (i.e., NaNO₃ loading $\simeq 9.3\%$), and then attained a plateau level. (e) The degree of weight loss at higher temperature decreased with the increases in NaNO₃ loading, and this weight loss disappeared for the sample containing more than 9.3% NaNO₃ (Fig. 1c). (f) XRD patterns of the thermally treated sample showed presence of NaCl (Fig. 3a). The intensities of NaCl peaks were proportional to the NaNO₃ loading, but became constant when NaNO₃ loading exceeded 9.3% (Na/ $Cl \approx 1$). (g) As-dried samples did not show NaCl peaks in XRD. They appeared at 250°C, slightly higher temperature than for the lower temperature weight loss process. (h) The NaNO₃ peaks could not be detected

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TABLE	
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Thermal Analysis of Alumina-Supported Mixture of RuCl₃ and NaNO₃

Sample No	Sample composition ^a	osition ^a	badad	w eigin	olumos							
.01	$RuCl_3 \cdot 3H_2O$	NaNO3	(mg)	at at	weight	Weigh	Weight loss ^c	/MP-)	$(-dW/dT)_{\max}^{d}$	Decomposition	osition	Melt
	(0/)	(0/)		(mg)	(giii)	140–310°C	310-400°C	Lower	Higher	of RuCl ₃	ICI3	or NaNO3
							(III)	2	2	Temp. (°C)	Peak height (μV)	Peak height (μV)
-	9.82 (4.04)	0.00 (0.00)	33.20	1.14	32.06	0.26 (0.22)	0.60 (1.30)	1	350	(334)	(1.6)	
2	9.77 (4.05)	1.13 (0.44)	32.50	1.24	31.31	0.59 (0.47)	0.53 (1.13)	267	387	I	I	ł
	9.63 (4.01)	2.11 (0.83)	33.60	1.12	32.48	0.56 (0.70)	0.41 (1.12)	239	388	230	0.5	ł
4	9.64 (4.05)	3.28 (1.30)	33.40	0.92	32.48	0.85 (0.97)	0.35 (0.87)	248	385	241	3.0	I
\$	9.36 (4.01)	6.33 (2.56)	32.95	1.16	31.79	1.54 (1.64)	0.31 (0.43)	255	380	250	6.0	1
9	9.31 (4.07)	9.29 (3.83)	33.25	1.65	31.60	1.88 (2.24)	0.26 (0.07)	225	l	220	5.5	0.6
٢	66.8	12.1	32.75	1.32	31.43	2.18 (2.15)	0.29 (0.07)	58	285	238	6.0	3.8
	(4.00)	(5.10)	32.55	1.19	32.06	1.86 (2.18)	0.24 (0.07)	253	294	249	8.0	4.5
80	8.74 (4.08)	18.7 (8.21)	33.30	1.42	31.88	2.19 (2.11)	0.55 (0.07)	236	1	240	6.7	10.0
a	8.32	26.4	33.25	1.22	32.03	2.18 (2.00)	0.62 (0.06)	226	Ι	231	8.5	16.2
n	(4.12)	(12.3)	33.50	1.18	32.32	2.12 (2.02)	0.59	232	ļ	232	7.2	15.8
10	7.47 (4 11)	39.6 (20.6)	33.00	1.08	31.92	1.80	0.48	235	I	241	8.0	31.0
Alumina		()-92 	33.20	0.48	32.72	0.24	0.09	I	I	I	Ι	

NOTES

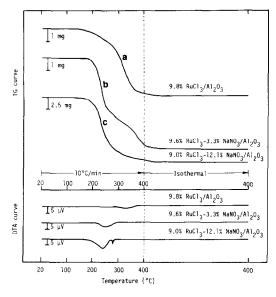


FIG. 1. Typical TG-TDA profiles.

for the thermally treated samples of low NaNO₃ loading; when NaNO₃ loading exceeded 9.3%, NaNO₃ peaks were detected and the intensity of the peaks increased with the increase in NaNO₃ loading.

These results suggest that RuCl₃ is decomposed by the following two reactions:

"RuCl₃" + NaNO₃
$$\xrightarrow{\text{process a}}$$
 RuO₂
+ NaCl (1)

$$"RuCl_3" \xrightarrow{\text{process } \mathbf{b}} RuO_2 \qquad (2)$$

The theoretical weight loss calculated based on Eq. (1) was in good agreement with observed degree of weight loss at the lower temperature. The theoretical amount of undecomposed NaNO₃ remained after process **a** was proportional to the intensity of the endothermic peak for melt of NaNO₃ detected by DTA at around 295°C for high NaNO₃ loading samples (Table 1).

Since commercial "RuCl₃ · $3H_2O$ " is a complex mixture of polynuclear Ru(IV) oxychloro species (21), detail mechanism for process **a** is not clear. However, it must be noted that whenever alkali-promoted Ru catalyst was prepared by impregnation of commercial "RuCl₃ · $3H_2O$ " and alkali or alkaline earth nitrate followed by thermal treatment and reduction, a process similar to process **a** produced alkali or alkaline earth chloride which cannot be removed by reduction, and that remaining chloride ion severely affects the catalyst performance (22).

Subsequent Reduction

In another series of experiments, samples were thermally treated at 400°C in the thermal analyzer and subsequent TPR profiles were examined on the same instrument. Maximum rates for the reduction of samples 1–6 were observed at about 160°C. This reduction temperature is slightly lower than reported temperature for bulk RuO₂ $(203^{\circ}C, (14))$ or RuO₂/SiO₂ (180°C, (16)). A higher loading of NaNO3 caused both a drastic rise in the reduction temperature and an increase in the intensity of the exothermic peak in DTA. Because the reduction temperature remained essentially constant unless NaNO₃ loading in the original sample exceeded 9.3% (i.e., Na/Cl \approx 1), increase in the reduction temperature for high NaNO₃-loading samples seems to be caused by the remaining NaNO₃ undecomposed by process a.

The XRD patterns for the reduced samples showed Ru metal peaks, and NaCl peaks were also seen in Na-containing samples (Figs. 2b and 3b). The peaks of NaNO₃ which could be observed for the thermally treated samples of high NaNO₃ loading disappeared in the reduced samples. However, sodium salts other than NaCl could not be detected by XRD except β -NaAlO₄ (23) found in samples 9 and 10.

The XRD peak height of Ru metal varied with Na content. This result was not caused by the presence of Ru species other than Ru metal, because the degree of weight loss at the reduction stage was essentially constant when NaNO₃ loading is less than 9.3%. Therefore, the peak height of Ru seems to reflect the particle size of Ru metal crystallites. To discuss the Ru particle size, the half-height width must be measured. However, as Ru peaks overlapped with alumina peaks, accurate half-height width could not be obtained even after subtraction of alumina peaks from XRD patterns of the sample. Therefore, Ru peak height was determined instead of the half-height width. Relative peak height of Ru(101) to γ - $Al_2O_3(440)$ was then calculated, and thus experimental variance in determining XRD was eliminated. As can be seen in Fig. 4, relative peak height of Ru metal decreased with the increase in Na/Cl ratio, and relative peak height of Ru metal reached minimum at Na/Cl = 1. In order to elucidate the effect of alkaline component on the particle size of Ru, the following experiments were carried out.

1. The sample 1 (9.8% $RuCl_3/Al_2O_3$) was heated at 250°C. A part of this sample was reduced with hydrogen on the thermal analyzer at 400°C. To the remaining part of the heated sample, NaCl was impregnated. The concentration of NaCl was adjusted to give the same concentration as sample 6. After drying in air, the sample was thermally treated in air at 400°C and reduced with hydrogen at 400°C.

2. The sample 6 $(9.3\% \text{ RuCl}_3-9.3\% \text{ NaNO}_3/\text{Al}_2\text{O}_3)$ was heated at 250°C. Using a part of this, TPR profile was examined and then XRD of the reduced sample was examined. The remaining part of the heated sample was washed with water repeatedly until no more chloride ions were detected in the supernatant. The sample was then dried in air. Thermal decomposition behaviour and subsequent TPR profile were examined.

Relative peak height of Ru became higher in the following order (sample No., thermal

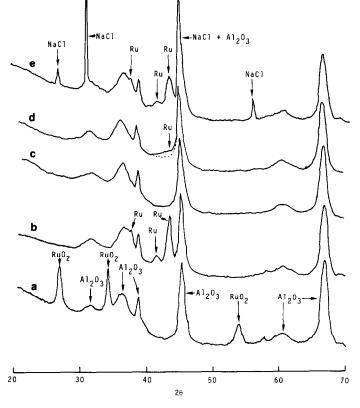


FIG. 2. XRD profiles of the samples derived from 9.8% RuCl₃/Al₂O₃ (Sample 1). They were prepared by (a) thermal treatment at 400°C; (b) thermal treatment at 400°C followed by reduction at 400°C; (c) heating at 250°C; (d) heating at 250°C followed by reduction at 400°C; (e) heating at 250°C, impregnation of NaCl, thermal treatment at 400°C, and subsequent reduction at 400°C.

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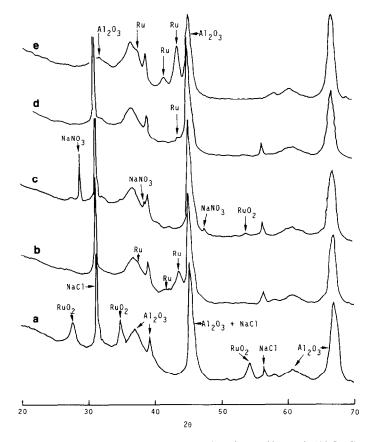


FIG. 3. XRD profiles of the samples derived from 9.3% RuCl₃=9.3% NaNO₃/Al₂O₃ (Sample 6). They were prepared by (a) thermal treatment at 400°C; (b) thermal treatment at 400°C followed by reduction at 400°C; (c) heating at 250°C; (d) heating at 250°C followed by reduction at 400°C; (e) heating at 250°C, removal of NaCl by washing with water, thermal treatment at 400°C, and subsequent reduction at 400°C.

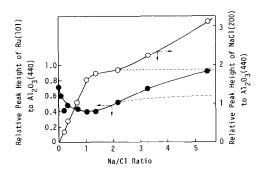


FIG. 4. Relation between Na/Cl ratio and relative peak heights of Ru(101) and NaCl(200) to $Al_2O_3(440)$ found in the XRD profiles of reduced RuCl₃-NaNO₃/ Al_2O_3 samples. Broken lines indicate peak heights corrected by taking into account of formation of NaAlO₂ from Al_2O_3 .

treatment temperature, and figure No. are given in this order; all samples were reduced at 400°C; other treatment was specified in parentheses):

1,250,2d < 6,250,3d < 6,400,3b < 1,(addition of NaCl),400,2e < 6,(removal of NaCl),400,3e < 1,400,2b.

When two samples prepared by the thermal treatment at 400 and 250°C are compared, Ru peak height of the former is much higher than the latter. This result indicates that during the thermal treatment sintering of RuO₂ particles occurs via the formation of volatile higher oxides of Ru (24, 25), and that sintering of Ru metal particles during reduction stage can be neglected under our reduction conditions. As the heating temperature 250° C is above the temperature for process **a**, RuCl₃ and NaNO₃ in sample 6 had been decomposed into RuO₂ and NaCl. Removal of NaCl from this sample promoted the aggregation of Ru particles. On the other hand, addition of NaCl to sample 1 prevented the aggregation of Ru particles. Therefore, we concluded that NaCl has a retarding effect on the sintering of RuO₂ during the thermal treatment stage. Consequently, the effect of NaNO₃ addition on the peak height of Ru (Fig. 4) can be explained along the same line because of the formation of NaCl by process **a**.

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